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thermochimica acta

Thermochimica Acta 443 (2006) 245–250

www.elsevier.com/locate/tca

# Solubility data for benzene in aqueous solutions of methyldiethanolamine (MDEA) and of diglycolamine (DGA)

Short communication

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Available online 24 February 2006

## **Abstract**

Specially designed equipment based on a static-analytic method with Rolsi<sup>TM</sup> pneumatic samplers for on line gas chromatograph analysis has been used for this work. Operating pressures and temperatures are between 0.3 and 10 MPa and between 293 and 393 K. Vapor pressures over liquid–liquid mixtures and benzene solubility data are reported herein for benzene with amine aqueous solutions (methyldiethanolamine (MDEA) and diglycolamine (DGA)). Modelling of solubility data is achieved using a simple model based on activity coefficients. © 2006 Elsevier B.V. All rights reserved.

*Keywords:* Solubility data; Methyldiethanolamine; Diglycolamine; Water; Benzene; Methane; Modelling

## **1. Introduction**

Aqueous alkanolamine solutions are used extensively for removal of acid gases in gas mixtures or liquefied petroleum gas (LPG). Some hydrocarbons particularly BTEX are absorbed in the amine solution and so industries need accurate hydrocarbon solubility data to develop new equation or correlations in order to design their absorption or liquid–liquid contactor units. BTEX quantities emissions have been specified by the Clean Air Act. Moreover, the benzene, toluene, ethylbenzene, xylene (BTEX) regulations obviously have considerable effect on most amine systems. Aromatics have particularly harmful effects in a sulfur plant feed. The amine treating units absorb appreciable quantities of aromatics from the feed gas. Aromatics are responsible of rapid loss of sulfur plant recovery efficiency, and consequently of frequent replacements of catalyst.

Key factors that affect sulfur catalyst deactivation are the amount of aromatics absorbed in the amine plant and the efficiency of aromatic destruction in the reaction furnace. This paper, first of a series, deals with benzene solubility in aqueous amine systems.

In this work, influence of various concentrations of MDEA and DGA (weight fractions from 0 to 0.5 and 0.7, respectively) on benzene solubility has been studied in presence of methane. DGA is a primary amine capable of removing not only hydrogen sulfide and carbon dioxide but also COS and mercaptans from gas and liquid stream [1]. MDEA is a tertiary amine which can be used to selectively remove H2S. CO2 hydrolyzes much slower than  $H_2S$  [1].

#### **2. Therm[odyn](#page-5-0)amic of the system**

[D](#page-5-0)ue to very low mutual solubilities in aqueous solvent–hydrocarbon systems, it is very easy to reach vapor–liquid–liquid equilibrium (VLLE) conditions. At high pressures the vapor phase in mainly composed of methane and benzene. The organic phase is composed mainly of benzene and methane. The aqueous phase is mainly composed of water and alkanolamine. Fig. 1 presents typical phase diagram of such a system. Consequently two hypotheses are done:

- There is no significant quantity of water or alkanolamine in organi[c phase.](#page-1-0)
- There is no significant quantity of water or alkanolamine in vapor phase.

Thus, for benzene, equilibrium thermodynamic equations are:

$$
x_2^0 \gamma_2^0 = x_2^w \gamma_2^w \tag{1}
$$

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#### <span id="page-1-0"></span>**Nomenclature**



$$
x_2^0 \Phi_2^0(T, P, x_2^0) = y_2 \Phi_2^v(T, P, y_2)
$$
  
\n
$$
\text{with } y_2^0 = \frac{\Phi_2^0(T, P, x_2^0)}{\Phi_2^{0*}(T, P)}
$$
\n(3)

The PSRK model [2] is used to calculate the activity coefficient and the composition of benzene in the organic phase.

## **3. Experi[ment](#page-5-0)al work**

#### *3.1. Materials*

The liquids chemicals have been used after distillation and careful degassing under a vacuum. The origin and purity of compounds are given in Table 1.



Fig. 1. Example of thermodynamic diagram in conditions close to described study.

#### *3.2. Apparatus and experimental procedures*

The apparatus used for the study is based on a static-analytic method with liquid and vapor phase sampling. This apparatus was described by Valtz et al. [3].

Three pressure transducers have been used for this work (Druck, model PTX 611) (nominal loads: 0.6, 4 and 6 MPa). They can be used up to 0.7, 5 and 7 MPa, respectively. They are therm[o reg](#page-5-0)ulated at fixed temperature (higher than the working temperature to avoid any condensation phenomenon).

Below 0.6 MPa, the calibration is performed against a pressure calibration device (Desgranges et Huot, model 24610). Between 0.3 and 7 MPa, it is done against a dead weight balance (Desgranges et Huot, model 5202 S CP). Uncertainty between  $1.4 \times 10^3$  Pa and 0.6 MPa is  $\pm 0.0001$  MPa. Uncertainty between 0.7 and 7 MPa is  $\pm$ 0.002 MPa.

Analytic methods are described in previous paper [3]. According to calibrations, uncertainty on benzene mole fraction is less than 2%.

### *3.3. Preparation of the aqueous amine solutions*

The compositions of aqueous solutions were prepared gravimetrically as described in Ref. [3].

## *3.4. Experimental procedure for benzene solubility measurements*

The evacuated equilibrium cell is loaded with about  $5 \text{ cm}^3$ of solvent (distilled water or aqueous amine solution). About  $2 \text{ cm}^3$  of benzene are added. In these conditions two liquid phases are present in the cell. At equilibrium, the total pressure is measured. Then the total pressure is increased up to about 0.5 MPa when necessary using methane. The solution is stirred vigorously for a long time, more than 1 h to achieve phase equilibrium. Steering speed is reduced for 1 h and samples of aqueous phase are withdrawn and analyzed by gas chromatography [4]. Several samples are analyzed to evaluate the repeatability of measurements.

## **4. Results**

#### *4.1. Solubility in water*

After loading the equilibrium cell, vapor pressure of the liquid–liquid mixture has been measured as a function of temperature. The results are presented in Ref. [3]. Anderson and Prausnitz [5] have measured the vapor pressure at seven temperatures. A very good agreement was found with our data. Methane is used to pressurize the system when sampling is not possible. The influence of meth[ane o](#page-5-0)n the benzene solubility [has](#page-5-0) been studied and already presented in Ref. [3]. Increasing methane pressure leads to decreasing benzene solubility. Consequently, extrapolation must be done to obtain the benzene solubility in the free of methane aqueous solution (see Fig. 2). Up to 0.5 MPa, methane has lo[w infl](#page-5-0)uence on benzene

<span id="page-2-0"></span>



Table 2

Vapor pressure over benzene—(MDEA  $(1)$  + water  $(2)$ ) for different amine concentrations



<sup>a</sup> Anderson and Prausnitz [5].

solubility (deviation less than 1% between benzene mole fractions calcul[ated](#page-5-0) by taking or not into account the methane contents). Several authors have studied the solubility of benzene in pure water [5–14]. As pointed out in Ref. [3] literature data appear a little dispersed, but close to the new data presented in Ref. [3].



#### Fig. 2. Determination of the benzene activity coefficient in water from measurement containing methane at 298.10 K. The vertical dashed line corresponds to the vapor pressure of the system without methane.  $(x)$  Extrapolated value for free of methane solution.

# *4.2. Solubility in aqueous MDEA solutions*

Vapor pressure over the liquid–liquid mixture (without methane) measured as a function of temperature is reported in Table 2. Solubility of benzene (see Tables 3 and 4) has been

Table 3 Benzene solubility in MDEA (1) + water (2) [with  $w_1 = 0.25$ ] mixture at various temperatures



*n*: number of samples analysed.

$$
\sigma = \left(\frac{n \times \sum x^2 - (\sum x)^2}{n \times (n-1)}\right)^{1/2}.
$$

<span id="page-3-0"></span>Table 4 Benzene solubility in MDEA (1) + water (2) [with  $w_1 = 0.5$ ] mixture at various temperatures

T(K)	P(MPa)	$x_2 \ (\times 10^4)$	$\boldsymbol{n}$	$\sigma (\times 10^4)$ 2	
298.10	0.5035	38	12		
298.14	2.501	31.9	8		
333.09	0.4992	69.1	12	3	
333.06	2.504	56.1	8	0.8	
363.19	0.5036	113	8	6	
393.32	0.5158	172	8	8	
393.27	2.456	163	10	8	
		$\left\langle n \times \sum x^2 - \left( \sum x \right)^2 \right\rangle$	1/2		

studied in two aqueous MDEA solutions (i.e. MDEA (1) + water

Vapor pressure over the liquid–liquid mixture (without methane) measured as a function of temperature is reported in Table 2. The solubility of benzene (see Tables 5 and 6) has been studied in two aqueous DGA solutions (i.e.  $DGA (1) + water (2)$ 

*n*: number of samples analysed.  $\sigma =$ n×  $\sum x^2$ −  $\left(\sum x\right)$  $\big)^2$  $n\times(n-1)$ .

(2) with  $w_1 = 0.25$  and 0.5).

with  $w_1 = 0.35$  and 0.7).

*4.3. Solubility in aqueous DGA solutions*

Table 5

Benzene solubility in  $(DGA(1) - water(2))$  [with  $w_1 = 0.35$ ] mixture at various temperatures

T(K)	P(MPa)	$x_2 \ (\times 10^4)$	n	$\sigma (\times 10^4)$	
298.22	0.5015	19.3	9		
298.21	2.486	15.6	10	0.5	
333.14	0.5041	31.4	8	2	
363.20	0.5052	47.3	9	2	
393.22	0.5025	75.5	8	3	

*n*: number of samples analysed. 
$$
\sigma = \left(\frac{n \times \sum x^2 - (\sum x)^2}{n \times (n-1)}\right)^{1/2}
$$

Table 6

Benzene solubility in (DGA (1) – water (2)) [with  $w_1 = 0.7$ ] mixture at various temperatures

.

.



*n*: number of samples analysed.  $\sigma$  =





Fig. 3. Vapor pressure parameters as a function of amine weight fraction.

Table 7 Vapor pressures parameters and deviations

Solvent	ΔT		$B(K^{-1})$		$D(x10^5T^{-E})$	BIAS(%)	AAD(%)
MDEA (1) + water (2) $(w_1 = 0.25)$	294.85-402.86	$-91.021$	$-522.4$	15.8965	$-2.1604$	0.27	0.36
MDEA (1) + water (2) $(w_1 = 0.5)$	291.80-393.35	$-268.194$	6460	43.4264	$-5.4759$	0.30	0.77
DGA (1) + water (2) $(w_1 = 0.35)$	292.16-393.92	$-243.460$	5177	39.7816	$-5.2494$	0.11	0.19
$DGA(1) + water(2)(w_1 = 0.7)$	293.14-393.99	$-723.763$	23338.1	114.8912	$-14.8608$	0.58	0.68





Vapor pressures can be represented with the following equation:

$$
\ln(P) = A + \frac{B}{T} + C\ln(T) + D \times T^{E}
$$
\n(4)

where *A*, *B*, *C*, *D* and *E* are parameters fitted on experimental data; they are reported in Table 7. These parameters appear as a function of amine weight fraction (see Fig. 3).

## **5. Discussion**

Eqs. (1)–(3) were used to [determ](#page-3-0)ine benzene activity coefficients in solvents. When enough isothermal experimental data are available, the activity coefficient can be calculated by extrapolation of the relationship between benzene activity coefficient [and pr](#page-0-0)essure (Fig. 2). Then, the solubility is determined with the following equation:

$$
x_2^{\mathrm{w}} = \frac{1}{\gamma_2^{\mathrm{w}}} \tag{5}
$$

The results are presented in Table 8. Fig. 4 presents the benzene activity coefficient as a function of temperature for all

Table 9 Parameters of Eq. (4) and corresponding deviations



Fig. 4. Benzene activity coefficient as a function of temperature. ( $\Delta$ ) Water, ( $\times$ ) MDEA water  $(25/75)$  wt.% mixture,  $(*)$  DGA water  $(35/65)$  wt.% mixture,  $(\bigcirc)$ MDEA water (50/50) wt.% mixture, ( $\Diamond$ ) DGA water (70/30) wt.% mixture.



Fig. 5. Benzene activity coefficient as a function of Amine concentration.  $(\bigcirc)$ Pure water,  $(\Delta)$  DGA,  $(\times)$  MDEA.

studied solutions. The first conclusion is that amine is a good solvent of benzene with solvent power increasing with temperature. Fig. 5 shows that the amine composition has more influence than the nature of the amine on benzene solubility. With respect to the previous conclusions, a simple model is developed in order to represent the activity coefficient of benzene in the aqueous solution. This model (see Eq. (6)) has a temperature second order polynomial form with parameters function of amine concentration.

$$
\gamma_2^{\text{w}}(T, X_{\text{amine}}) = A \times T^2 + B \times T + C \tag{6}
$$

The corresponding parameters reported in Table 9. Combining Eqs. (5) and (6), allows calculating benzene solubility in any aqueous amine solution for the amine  $(1)$  + water  $(2)$  system in the 0–0.7 weight fraction range.



## <span id="page-5-0"></span>**6. Conclusion**

The specially designed equipment based on a static-analytic method with Rolsi<sup>TM</sup> pneumatic samplers for on line gas chromatograph analysis has been operated to get benzene solubility data between 0.3 and 10 MPa and between 293 and 393 K. Vapor pressures over liquid–liquid mixtures are reported herein for benzene with amine aqueous solutions (methyldiethanolamine (MDEA) and diglycolamine (DGA)). They are successfully represented using DIPPR type equation (deviations less than 1%). Modelling of solubility data has been achieved using a simple model based on activity coefficients. Amine has been found as a good solvent of benzene with solvent power increasing with temperature. Amine composition has much more influence than the nature of the amine on benzene solubility.

## **Acknowledgments**

The authors want to thank the Gas Processors Association for its financial support and the Members of Enthalpy Steering Committee for fruitful discussions and in particular Dr. Mike Hegarty.

### **References**

- [1] Engineering Data Book, SI Version, Gas Processors Association, 11th ed., 1998.
- [2] T. Holderbaum, J. Gmehling, Fluid Phase Equilib. 70 (1991) 251– 265.
- [3] A. Valtz, M. Hegarty, D. Richon, Fluid Phase Equilib. 210 (2003) 257–276.
- [4] P. Guilbot, A. Valtz, H. Legendre, D. Richon, Analysis 28 (2000) 426–431.
- [5] F. Anderson, J. Prausnitz, Fluid Phase Equilib. 32 (1986) 63–76.
- [6] D.M. Alexander, J. Phys. Chem. 63 (1959) 1021-1022.
- [7] D.S. Arnold, C.A. Plank, E.E. Erickson, F.P. Pike, J. Chem. Eng. Data 3 (1958) 253.
- [8] H. Chen, J. Wagner, J. Chem. Eng. Data 39 (1994) 470–474.
- [9] F. Franks, M. Gen, H.H. Johnson, J. Chem. Soc. Lond. (1963) 2716–2723.
- [10] P.M. Gross, J.H. Saylor, J. Am. Chem. Soc. 53 (1931) 1744– 1751.
- [11] R.A. Pierotti, A.A. Liabastre, Report PB 211163, Atlanta, 1972.
- [12] R.M. Plenkina, N.V. Kuzyakina, I.A. Markina, Khim. Prom. Moscow 7 (1989) 20.
- [13] G. Tagliavini, G. Arich, Ricerca Sci. 12 (1958) 2557–2561.
- [14] V.V. Udovenko, L.P. Aleksandrova, Zh. Fiz. Khim. 37 (1963) 52.